

# DESIGN OF TEMPERATURE CALIBRATION LOADS AND IMPEDANCE MATCHING TO FREE SPACE

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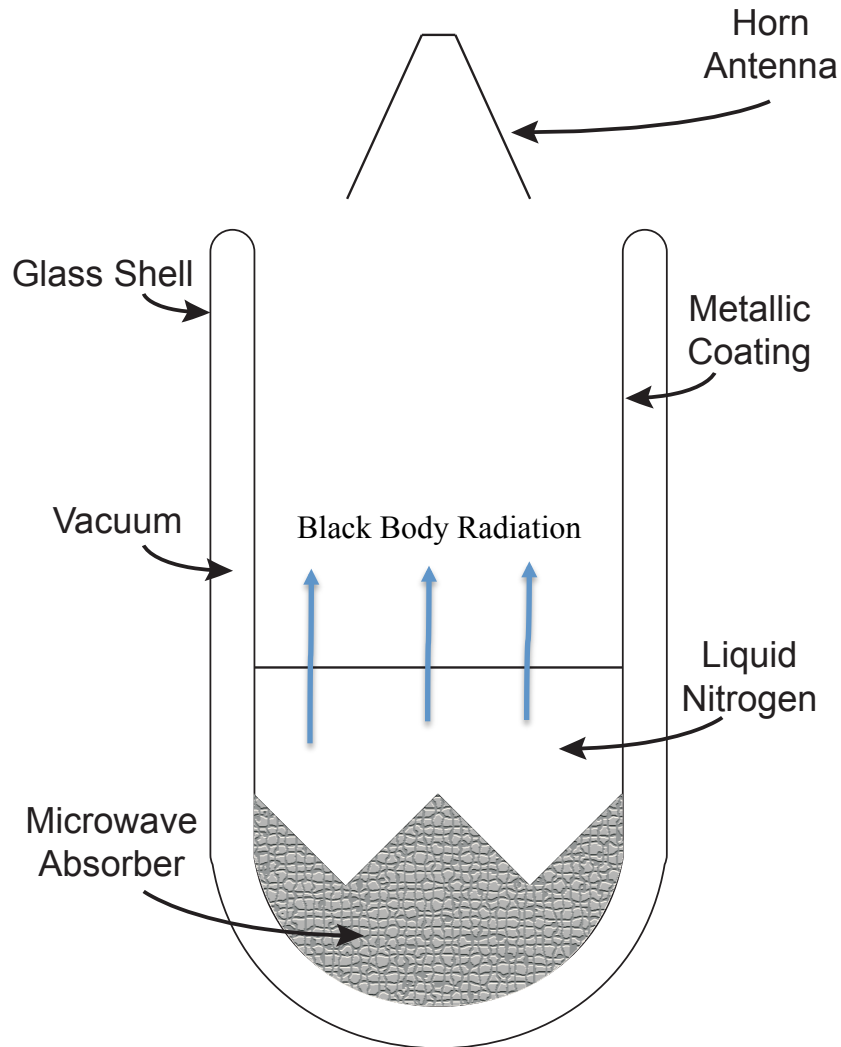
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# CALIBRATION SOURCES AT AMBIENT AND LIQUID NITROGEN TEMPERATURES

- Need two blackbody radiation sources that can couple to a microwave receiving antenna.
- The two sources must have exactly known temperatures.
- Liquid nitrogen (LN2) slowly boils in the Dewar flask to maintain its temperature at the boiling point of 77 K
- The microwave absorbing material in the LN2 liquid radiates as a black body.
- The black body source has a pyramidal surface to avoid plane wave reflections at the surface.
- Some experimenters use a large open sheet of pyramidal absorber for the ambient temperature source.
- Some use absorbing material in a metal cylinder of similar dimensions to the LN2 source.
- Ambient temperature is measured with a thermometer inside the absorber material.

# LIQUID NITROGEN TEMPERATURE CALIBRATION



- Dewar Flask acts as a waveguide
- Boiling liquid nitrogen (LN2) @ 77 K
- Absorber acts as 77K black body
- Bensadoun et al. used numerous mylar and fiberglass windows to prevent condensation and control IR radiation into the dewar.
- I have found that you can do without windows for short measurement runs lasting less than 30 minutes.
- Boiling LN2 gives off absolutely dry nitrogen gas keeping moisture out.

This design was adapted from an article by Bensadoun et al. (1992) Smoot group

# HOME MADE ABSORBER SURFACE



- Absorber material must have a pyramidal surface otherwise you get reflections leading to cavity resonances in the Dewar Flask.
- I have made a pyramidal surface using ½" flat absorber sheet glued with superglue.
- This configuration works well in the tests described here.



# CUMING MICROWAVE

Technical Bulletin 390-1A

## C-RAM SFC-HP

### VERY HIGH PERFORMANCE BROADBAND PYRAMIDAL RF ABSORBER

RoHS  
Compliant

Pyramidal microwave absorber material is available from numerous sources. Cuming sells their materials on their website, [www.cuming.com](http://www.cuming.com)

C-RAM SFC-HP is a series of very high performance broadbanded RF absorbers made from specially treated low density polyurethane foam. The product is flexible and tolerant of physical abuse. Using a very steep pyramid design which provides an impedance gradient, C-RAM SFC-HP provides improved premium performance in anechoic chambers at both normal and off-normal incidence angles. These products meet all of the fire retardancy requirements of NRL Specification 8093 tests 1, 2, and 3, MS-8-21 tests 1, 2, and 3, and T.I. drawing 2693066, as well as ASTM E-84-97a, Class A.

#### TYPICAL PROPERTIES

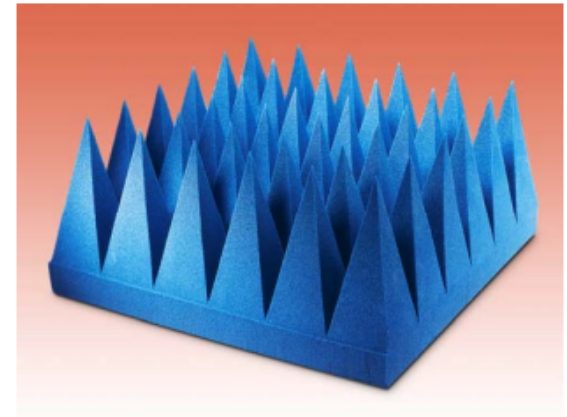
Typical weights, dimensions, and reflectivities of the various grades of C-RAM SFC-HP are given in the tables on the reverse side.

Typically, C-RAM SFC-HP absorbers can handle up to  $1.0 \text{ W/in}^2$  ( $1.5 \text{ kW/m}^2$ ) of RF energy in a temperature controlled room, but this is dependent upon frequency and application.

The product is black throughout, and generally is sprayed with a light blue surface coating, both for cleanliness and to provide better light reflection inside a chamber. The absorber can be left unpainted if requested.

#### AVAILABILITY

Standard sizes of C-RAM SFC-HP are listed in Table 1, ranging from 8 to 36 inch height. Are shaped as conventional pyramids and supplied as square 24 inch (610 mm) panels.



In addition to simply supplying a bill of materials, Cuming Microwave designs and installs complete anechoic chambers. Chambers can be designed to meet your specifications, and an entire kit of materials is supplied, including factory pre-cuts of special fitting parts. We can install all materials or supply technical support to help you complete your own installation.

# IMPEDENCE MATCH OF CALIBRATION SOURCES AND SPACE

- An issue arises with the process of using two calibration sources and a deep space background measurement
- All three must have same impedance match to the detector
- A result of the mismatch is standing waves in the waveguide
- Of course there are no reflections when pointed at the sky
- These effects can introduce errors.
- Two principle effects
  - Preamplifier gain is sensitive to the impedance match. Must be the same for each condition.
  - Standing wave patterns make it difficult to reposition the antenna

# IMPEDANCE MATCH TESTS

- Tested two different configurations
  - LNB from Dish Network antenna
  - Kuhne electronics 10.3 GHz preamp and transverter

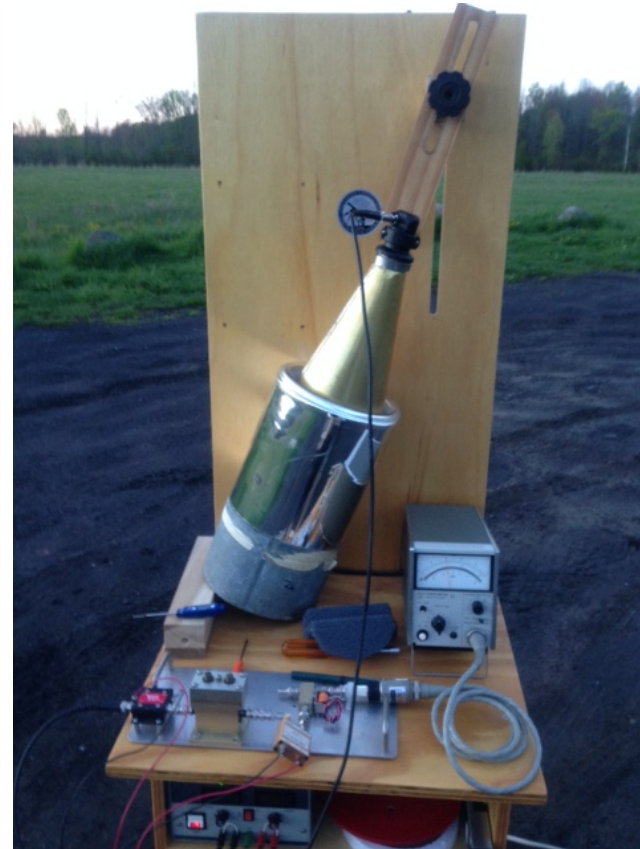
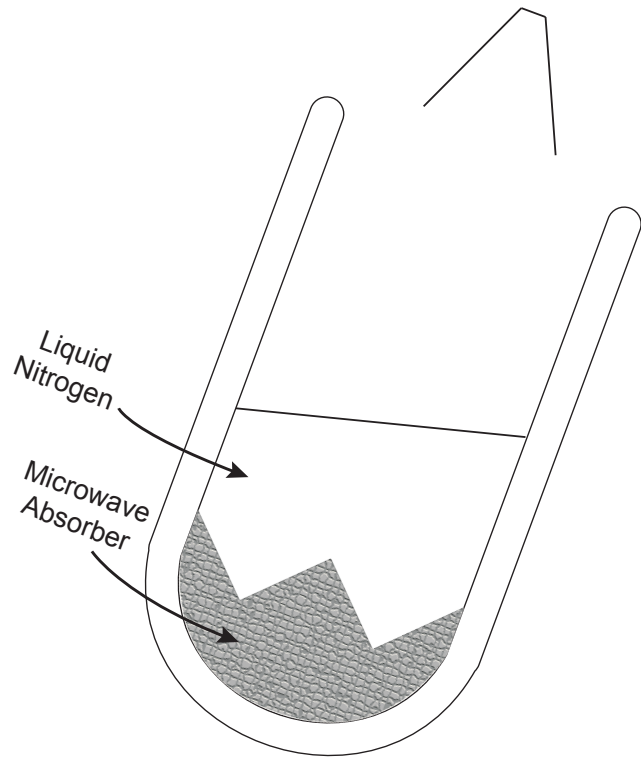
Standing waves occur only in LN2 filled dewar.

Due to plane wave reflections from the air-LN2 surface

LN2 has an index of refraction of 1.2 at 10 GHz

- The Kuhne system had weaker reflections than the dish network system
- For dish network horn It was possible to eliminate reflections by tilting Dewar flask

## TILTED COLD LOAD DEWAR

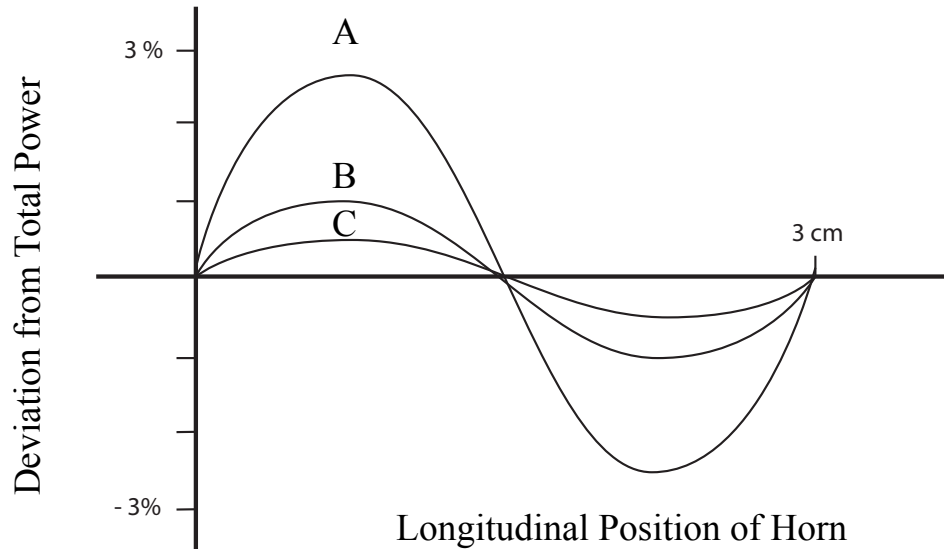


- Tilting the dewar changes the angle of the interface and substantially reduces the formation of standing waves.



# INTERFACE INTERFERENCE

Interference causes peaks and valleys as you move horn antenna longitudinally.



- Reflection is reduced by
  - Tilting LN2 interface
  - Using the proper polarization orientation
  - This only works with microwaves of a single polarization

A – Axis of antenna normal to LN2 surface

B – LN2 surface tilted at 20 degrees

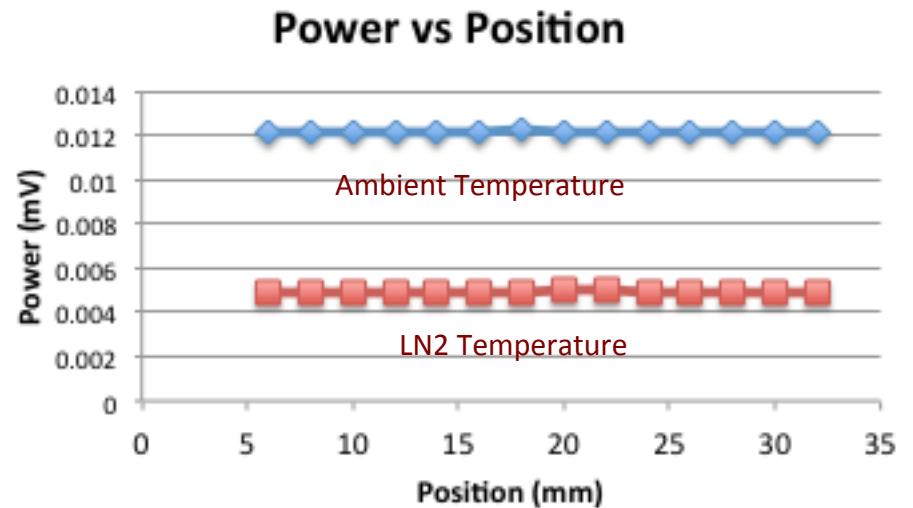
C – Tilted 20 degrees and polarization in the plane of incidence as in Brewster's angle.

Brewster's angle = 32 degrees. May be difficult to tilt Dewar that far. The 0.5% peaks at 20 degrees of tilt are barely detectable on the analog meter. This procedure substantially improves the reproducibility of the cold load calibration.

# COMMERCIAL PREAMPLIFIER PERFORMANCE



- Kuhne MKU 102 S EME preamp and 10 MKU G4 transverter at 10.3 GHz input
- Mounted antenna on sliding table with digital position gauge
- Measured noise vs longitudinal position
- There are no standing waves at ambient or LN2 temperature
- This means that there is the same match as free space



No need to tilt Dewar with this configuration